

SRR Loaded UWB Monopole Antenna with WiMAX and WLAN Notch

Shiney Thankachan, Anju A Chandran

Abstract— This paper presents a compact sized coplanar waveguide fed (CPW) printed circular monopole antenna for ultra wideband (UWB) communications having WiMAX and WLAN frequency notch. The proposed antenna achieved dual frequency notching by loading circular split ring resonator (SRR) on a low cost FR4 Epoxy substrate. The electromagnetic inductive coupling of the SRR with the CPW provides the frequency notch. The antenna's return loss and VSWR plots are presented here to confirm the notching.

Index Terms—CPW feed, Monopole antenna, UWB, SRR, WiMAX, WLAN

I. INTRODUCTION

Communication systems have increased the demand for cost effective, compact antennas with interference reduction capabilities. According to federal communication commission (FCC) rules, from 2002 onwards the 3.1 - 10.6 GHz band is allocated to the ultra wideband (UWB) applications [1]. UWB technology has several advantages like very wide bandwidth ranging from 3.1 to 10.6 GHz compared to most of the existing wireless communication standards and low cost, simple RF circuitry, high data rates and low average radiated power. To reduce interference between ultrawideband (UWB) systems and other narrow band systems, several designs are available in open literature. Notch characteristics achieved by changing the shapes of radiator with various types of slot or by parasitic loading [2]–[6]. Several design configurations include triple notch frequencies [7], double notch frequencies [8] and single notch frequencies [9] achieved using various design configurations employed within printed planar monopole antennas. Other design configurations are dual-frequency notch and wideband notch filtering by loading SRR pair on the back side of CPW-fed monopole antenna [10]–[11].

This paper presents a simple method to design a frequency notched UWB antenna by loading single ring dual SRRs on the back side of a CPW fed printed circular monopole antenna. The single ring SRRs are placed symmetrically on the opposite surface of the printed planar monopole antenna along the signal line which results in a notch frequency. Resulting notch frequency changes in accordance with the dimensions of circular SRRs. Propagation of electromagnetic

(EM) signals, with their magnetic fields along the axes of the SRR's, interacts with the SRRs, and causes the SRRs to

operates as magnetic dipoles. The propagating EM signal induces an electro motive force on the SRR, which in turn induces oscillating current within the circular ring SRR [12]. At a particular frequency which corresponds to the dimensions of SRR yields a resonance and prohibits signal propagation at this resonance frequency. When the excitation is given the propagating signal is rejected and reflected back, which yields a feeble radiation at the desired notch frequencies. Multiple notches can be achieved by loading multiple SRR with different geometrical dimensions.

In this paper simulated results are demonstrated as 3 different sections such as antenna with 3.5GHz WiMAX notch, antenna with 5.5GHz WLAN notch and by combining these two in a single printed circular monopole antenna giving dual frequency notch. Here we proposed frequency notching technique using circular single ring SRR, which yields a notching at a single frequency [13]. In most of the previous methods described earlier, where most of the modifications and incorporations are on the ground plane or radiator. The simplicity of our design is that here there is no need of varying the shape of radiator and ground plane and it can also be employed in any CPW-fed planar monopole UWB antenna.

II. ANTENNA CONFIGURATIONS

Schematic of the proposed antenna with dual frequency notch is shown in Fig.1. The proposed antenna is fabricated on FR4 Epoxy material having relative permittivity, $\epsilon_r=4.4$, $\tan\delta=0.02$, and thickness $h=1.6mm$. The circular uwb monopole having radius $R=12.5mm$ is fed by a CPW consisting of ground planes having widths $W_1=22mm$ and $W_2=22mm$, length $L_s=29.4mm$ and a signal line having length $L_s+t=29.6$ and width $S=5mm$. The slots between the signal line and ground planes have width $S_g=0.5mm$. Antenna loaded with two circular shaped single ring split ring resonators, shown in Fig. 1(c), where r is the radius of the SRR, conductor width w and the split gap g . Circular shaped single ring SRRs of two different dimensions are printed on the opposite surface of a CPW separated by the substrate height, as shown in Fig. 1(b). A single ring SRR is shown in Fig. 1(c) having dimensions r_i , which is radius of SRR, conductor thickness w_i , and split gaps g_i , where $i=1,2$, corresponding to the SRR 1 and 2, respectively. Where $r_1=7.2mm$, width $w_1=0.5mm$ and split gap $g_1=0.5mm$, the SRR corresponds to 3.5GHz WiMAX and $r_2=5mm$, width $w_2=0.5mm$ and split gap $g_2=0.5mm$, which corresponds to 5.5GHz WLAN frequency. According to the design

Manuscript received July, 2016.

Shiney Thankachan, Assistant Professor, Department of ECE, College of Engineering Kidangoor, Kottayam, Kerala, India, Phone.No:9496826575

Anju A Chandran, PG Student, Department of ECE, College of Engineering Kidangoor, Kottayam, Kerala, India, Phone.No:9961227257

equations of SRR, each SRR's resonance frequency varies which depends on its geometrical dimensions [14].

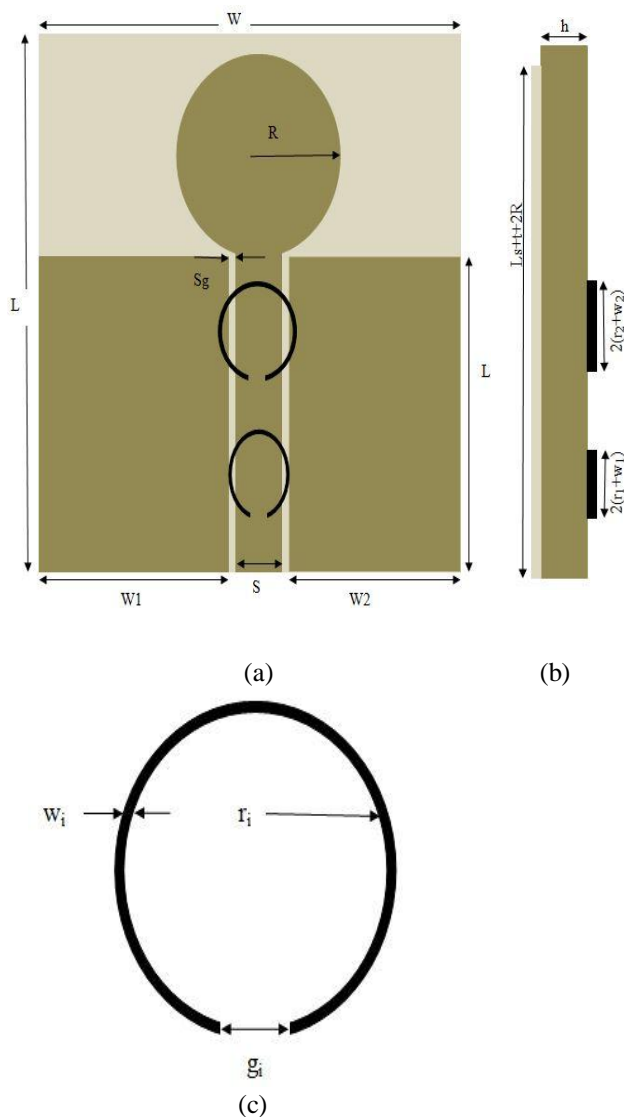


Fig. 1. (a) Schematic of a printed circular monopole fed by CPW: Top view with SRR printed in the back side (b) Side view of the printed circular monopole antenna fed by CPW loaded with SRRs (c) Schematic of circular SRR having dimensions r_i , w_i and g_i , where $i=1,2$ corresponding to SRR 1 and 2

III. RESULTS AND ANALYSIS

A CPW fed circular monopole uwb antenna without SRRs and with SRRs to obtain dual frequency notches is simulated on FR4 substrate having thickness $h=1.6\text{mm}$ and dielectric constant $\epsilon_r=4.4$. Here the antenna is simulated as three steps - During the first step by loading a single SRR having dimensions that corresponds to 3.5GHz WiMAX frequency, in second step by loading a single SRR having dimensions that corresponds to 5.5GHz WLAN frequency and in third by loading dual SRR to obtain dual frequency notch. The simulated results show a close corresponds with the theoretical results. The prototypes were designed and simulated using a commercial EM simulator that is HFSS.

A. Simulated return loss characteristics

Fig. 2 shows the simulated magnitude of the return loss (reflection coefficient) of the circular monopole uwb antenna

without loading SRRs with design parameters described in Table I. It can be seen from the figure; the CPW fed circular monopole UWB antenna without any SRR loading operates for the entire UWB bandwidth, and have return loss less than -10db .

Fig. 3 shows the simulated magnitude of the return loss (reflection coefficient) of single SRR loaded circular monopole uwb antenna giving notches at 3.5GHz, frequency corresponds to the SRR geometric dimensions. It can be seen that, return loss is above -10db at this particular frequency. Fig.4 shows the simulated magnitude of the return loss (reflection coefficient) of single SRR loaded circular monopole uwb antenna giving notches at 5.5GHz, frequency corresponds to the SRR geometric dimensions. It can be seen that, return loss is above -10db at this particular frequency.

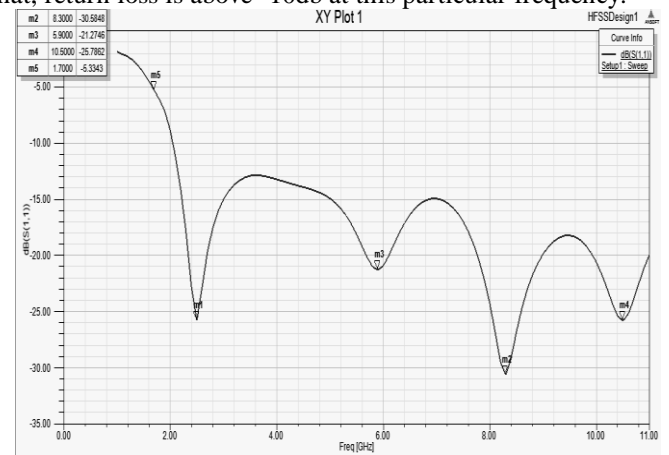


Fig.2. Simulated S11 plot of CPW Fed Circular UWB Monopole Antenna

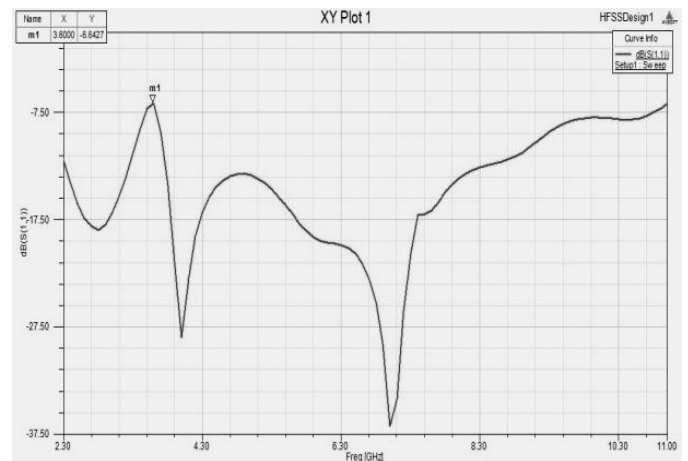


Fig.3. Simulated S11 plot of CPW Fed Circular UWB Monopole Antenna with 3.5GHz notch

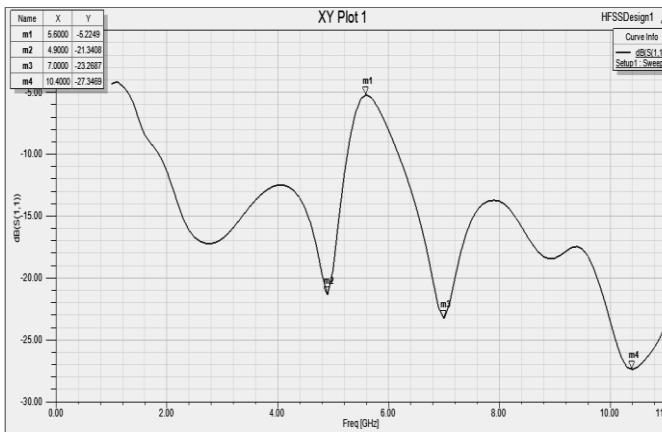


Fig.4. Simulated S11 plot of CPW Fed Circular UWB Monopole Antenna with 5.5GHz notch

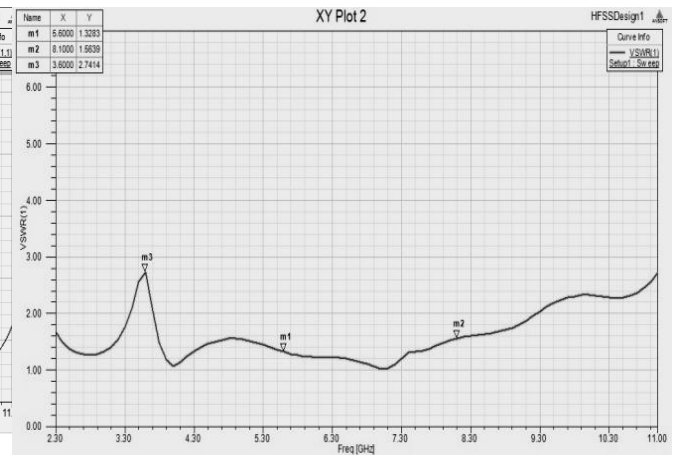


Fig.7 VSWR of CPW fed circular monopole UWB antenna with 3.5GHz notch

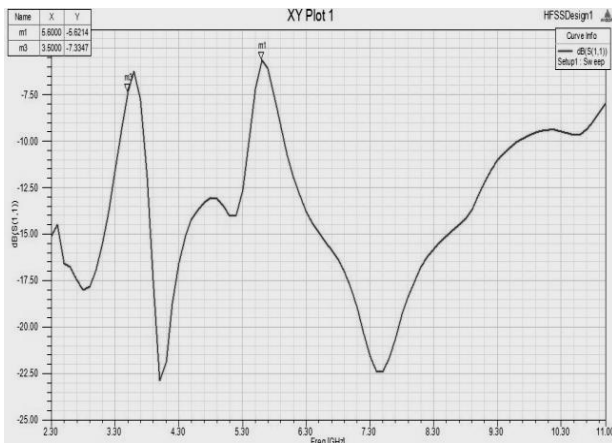


Fig.5. Simulated S11 plot of CPW Fed Circular UWB Monopole Antenna with dual frequency notch

Fig.5 shows the simulated magnitude of the return loss (reflection coefficient) of dual SRR loaded circular monopole uwb antenna giving notches at 3.5GHz and 5.5GHz.

B. Simulated VSWR characteristics

The voltage standing wave ratio (VSWR) plot of the circular monopole UWB antenna is shown in Fig.6, from which it is observed that VSWR values are less than 2 in the entire bandwidth. Fig.7 shows the VSWR plot of single SRR loaded circular monopole UWB antenna having VSWR above 2 at desired 3.5GHz frequency.

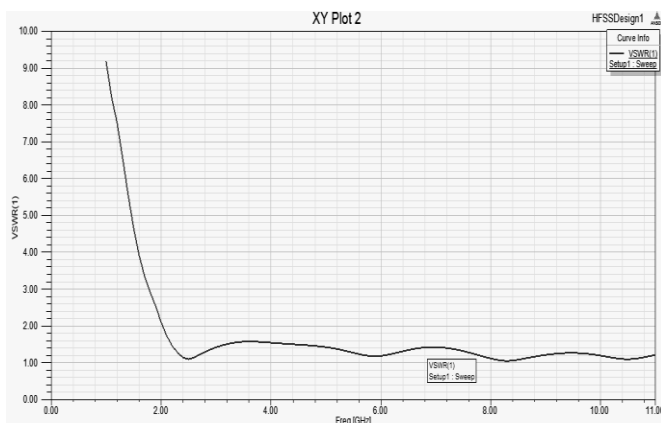


Fig.6 VSWR of CPW fed circular monopole UWB antenna

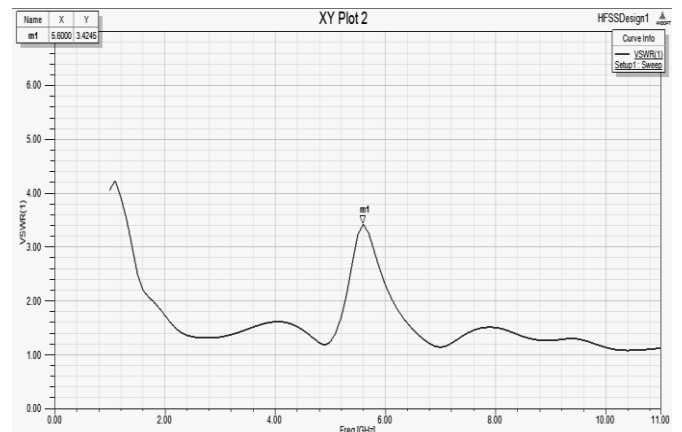


Fig.8 VSWR of CPW fed circular monopole UWB antenna with 5.5GHz notch

Fig.8 shows the VSWR plot of single SRR loaded circular monopole UWB antenna having VSWR above 2 at desired 5.5 GHz frequency. Fig.9 shows the VSWR plot of single SRR loaded circular monopole UWB antenna having VSWR above 2 at two desired notching frequencies.

C. Simulated Gain characteristics

Fig.10 shows the simulated gain plot of circular SRR loaded UWB circular monopole antenna with dual notch characteristics that is at 3.5GHz and 5.5GHz. It can be observed from the plot that at the two specified notching frequencies the gain is very low compared to other frequencies in the UWB spectrum.

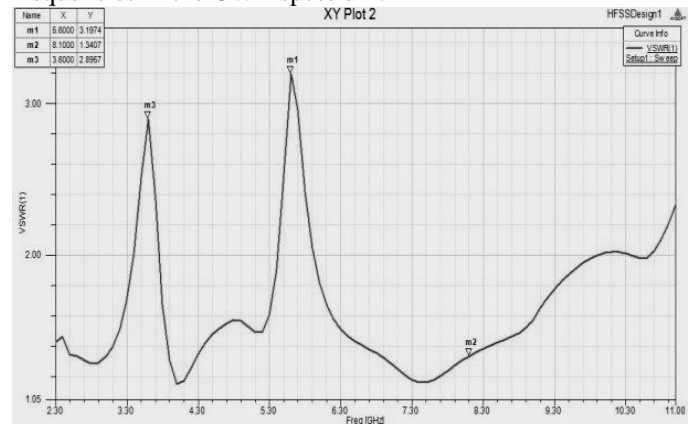


Fig.9 VSWR of CPW fed circular monopole UWB antenna with dual frequency notch

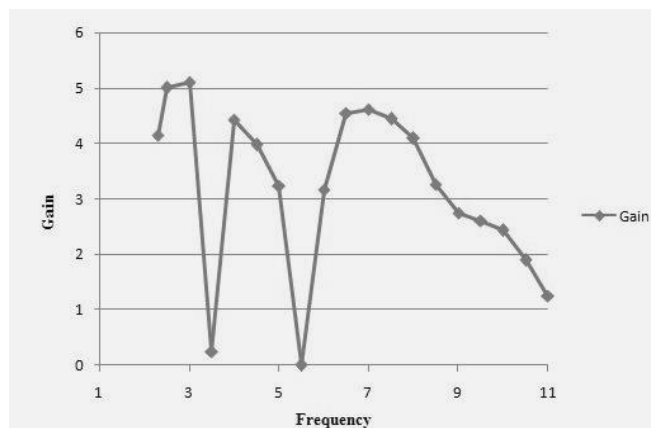


Fig.10 Gain plot of CPW fed circular monopole with dual notch

IV. CONCLUSION

A CPW fed circular monopole UWB antenna loaded with circular SRR's exhibiting dual frequency notch characteristic has been proposed and presented here. The configuration works with accurate lacing of the SRR on the opposite surface of the CPW feed line. The electromagnetic inductive coupling between the SRR and the feed line at its resonance frequency produce the desired frequency notching. The antenna dimensions and the SRR dimensions are independent of each other. The notch frequency can be varied to the desired value by varying the SRR dimensions based on the design equations.

ACKNOWLEDGMENT

Authors are grateful to the TEQIP, College of Engineering Kidangoor for the financial support to complete this work.

REFERENCES

- [1] Hedayat Rousta, Mohammad Naser-Moghadasi, and Bal S. Virdee, "Compact UWB Planar Monopole Antenna", *IEEE Antennas and wireless propagation letters*, VOL. 8, 2009
- [2] Y. Zhang *et al.* "Planar ultrawideband antennas with multiple notched, bands based on etched slots on the patch and/or split ring resonators on the feed line," *IEEE Trans. Antennas Propag.*, vol. 56, no. 9, pp. 3063–3068, Sep. 2008.
- [3] P. Wang, G. J. Wen, Y. H. Sun and , Y. J. Huang. "Compact CPW-fed planar monopole antenna with distinct triple bands for WiFi/WiMAX applications," *Electron. Lett.*, vol. 48, no. 7, pp. 357–359, Mar. 2012.
- [4] D. Jiang, R. Xu, W. Lin, and Y. Xu, "Compact dual-band-notched UWB planar monopole antenna with modified CSRR," *Electron. Lett.*, vol. 48, no. 20, pp. 1250–1252, Sep. 2012.
- [5] W. Jiang and W. Che, "A novel UWB antenna with dual notched bands for WiMAX and WLAN applications," *IEEE Antennas Wireless Propag. Lett.*, vol. 11, pp. 293–296, 2012.
- [6] M.-C. Tang *et al.*, "Compact UWB antenna with multiple band-notches for WiMAX and WLAN," *IEEE Trans. Antennas Propag.*, vol. 59, no. 4, pp. 1372–1376, Apr. 2011.
- [7] W. T. Li, X.W. Shi, and Y. Q. Hei, "Novel planar UWB monopole antenna with triple band-notched characteristics," *IEEE Antennas Wireless Propag. Lett.*, vol. 8, pp. 1094–1098, 2009.

- [8] Q.-X. Chu and Y.-Y. Yang, "A compact ultrawideband antenna with 3.4/5.5 GHz dual band-notched characteristics," *IEEE Trans. Antennas Propag.*, vol. 56, no. 12, pp. 3637–3644, Dec. 2008.
- [9] C.Y. Hong, C.W. Ling, I. Y. Tarn, and S. J. Chung, "Design of a planar ultrawideband antenna with a new band-notch structure," *IEEE Trans. Antennas Propag.*, vol. 55, no. 12, pp. 3391–3397, Dec. 2007.
- [10] J. Y. Siddiqui, C. Saha, and Y. M. M. Antar, "Compact SRR loaded UWB circular monopole antenna with frequency notch characteristics," *IEEE Trans. Antennas Propag.*, vol. 62, no. 8, pp. 4015–4020, Aug. 2014.
- [11] J. Y. Siddiqui, C. Saha, and Y. M. M. Antar, "Compact Dual SRR loaded UWB monopole antenna with dual frequency and wideband frequency notch characteristics," *IEEE antennas and wireless propagation letters*, vol. 14, 2015.
- [12] R. Marqués and F. Martín, "Split ring resonators and related topologies," in *Theory and Phenomena of Metamaterials*, F. Capolino, Ed. Boca Raton, FL, USA: CRC Press, 2009, ch. 16.
- [13] J. D. Baena, R. Marques, J. Bonache, F. Martín, F. Falcone, T. Lopetegi, M. Beruete, M. A. G. Laso, J. Garcia, M. Sorolla, and F. Medina, "Modified and complementary split ring resonators for metasurface and metamaterial design," in *Proc. 10th Bianisotropics Conf.*, Ghent, Belgium, 2004, pp. 168–171.
- [14] Jamel BT, Mondher L and Fethi ,C" A New Proposed Analytical Model of Circular Split Ring Resonator". 2011 *Journal of Materials Science and Engineering B1*, pp. 696-701.

First Author

Mrs. Shiney Thankachan

Assistant Professor, Electronics and Communication Department, College of Engineering Kidangoor, Kottayam.

Second Author



Ms. Anju A Chandran received her BTech Degree in Electronics and Communications engineering From CUSAT, Kerala, India in 2013. She is currently pursuing her MTech Degree in Wireless Technology from CUSAT, Kerala, India. Her areas of interest include UWB Antenna Design.