

# Multi Storied ( G + 5) Furniture Showroom Building , Seismic Load Manual Calculation

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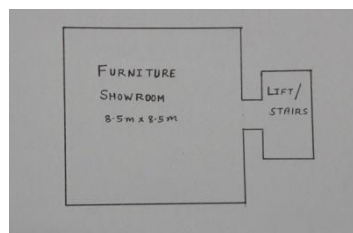
**Abstract** –The rapid growths of urban population, the high cost of land, the desire to avoid a continuous urban sprawl and the need to preserve important agricultural production have consequent pressure on limited space and these all contributed to drive buildings upward. As the height of building increase, the lateral load resisting system becomes more important than the structural system that resists the gravitational loads. As earthquakes can happen anywhere, some measure of earthquake resistance in the form of reserve ductility and redundancy should be built into the design of all structures to prevent catastrophic failures.

*Index terms* - Seismic Analysis, High rise building, Base Shear,

## 1.INTRODUCTION

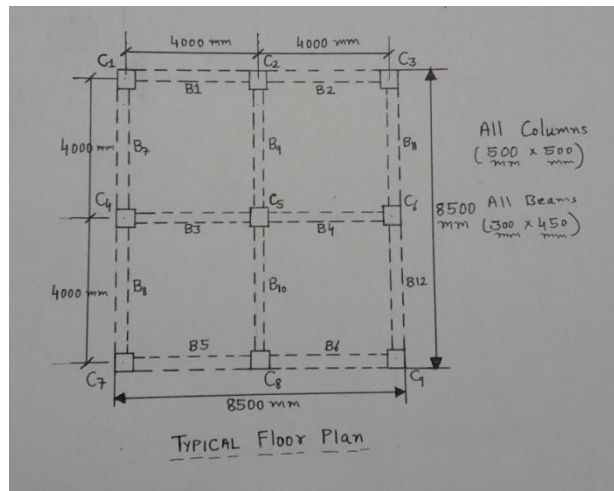
The important objective of engineers is to design and build a structure in such a way that damage to the structure and its structural component during the earthquake is minimized. Seismic analysis is a major tool in earthquake engineering which is used to understand the response of buildings due to seismic excitations in a simpler manner . This G + 5 furniture showroom building is analyzed for earthquake load. In seismic load analysis, we adopt Indian standard code of practice IS-1893 (Part I: 2002) guidelines and methodology. The horizontal forces due to earth quake are assumed to act at each of the floor levels and they induce axial forces in the columns and bending moments in all the members of the frame.

## 2. PLAN OF G + 5 STRUCTURE



This Showroom building consisting of two blocks, one is functional block (Show-

room) and another is service block (Lift / Stairs etc ). The Lift / Stairs block is structurally independent of Show room block .



The typical floor plan of G + 5, furniture showroom building of area 72.25 sq.m. proposed in Jaipur is shown above .

### 3.STRUCTURE ANALYSIS

Our building is situated in Jaipur. Height of each story is taken 3.5 meter. Height of column from plinth beam bottom to footing top is 1mtr. Showroom building rest on medium soil. Slab thickness of each story is 125mm. Brick masonry walls are 230mm thick and plaster thickness including both side is 25mm. As per I.S. 1893( Part –I ):2002 the design seismic base shear  $V_B$  which is nothing but the total design lateral force along any principal direction shall be determined by  $V_B = A_h W$  , Where  $A_h$  is the design horizontal spectrum value given by  $A_h = \frac{ZI}{2R} \left( \frac{S_a}{g} \right)$  . As Jaipur lie in zone II , so zone factor  $Z= 0.1$ ; Importance factor  $I$  for our building is 1. Our building is ordinary RC moment resisting frame building with brick infill panels , thus Response reduction factor  $R=3$  . As per I.S. 1893( Part –I ):2002 , the approximate fundamental natural period of vibration ( $T_a$ ) for our building is given by formula  $T_a = \frac{0.09h}{\sqrt{d}} = 0.09 * 21.225/ (8.5)^{1/2} = 0.655$  sec and  $\frac{S_a}{g} = \frac{1.36}{T} = 2.076$ . By substituting values in formula ,we get  $A_h = 0.0346$  , thus  $V_B = 0.0346 W$  .

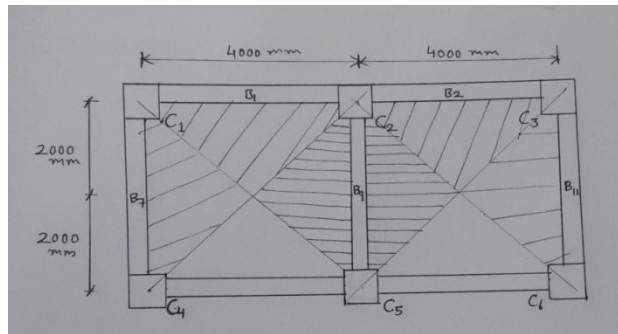
We analyze external frame  $C_1 - C_2 - C_3$  :

Total seismic weight  $W$  for this frame is calculated by summing the seismic weight of concerning columns  $C_1, C_2$  and  $C_3$  . We take live load on all floors is  $4\text{KN/m}^2$  and floor finish load is  $1\text{kn/m}^2$ . Thus seismic weights  $W_1, W_2$  and  $W_3$  is calculated by summing full D.L. and only 50% of L.L.

While calculating seismic weights, from simplicity point of view, we take same load at all floors including roof and G.F.

**CALCULATION FOR TYPICAL FLOOR :**

(A)Load per unit area of terrace slab	DL	LL
r.c.c. slab self weight	[ 3.125 + 0.0 ] $\text{kn/m}^2$	
{ $25\text{KN/m}^3 * 0.125\text{m}=3.125 \text{KN/m}^2$ }		
floor finish	[ 1.0 + 0.0 ] $\text{kn/m}^2$	
live load	[ 0.0 + 4.0 ] $\text{kn/m}^2$	
Sum =	[ 4.125 + 4.0 ] $\text{kn/m}^2$	



(B) Load taken by Beam  $B_1$ ( In our case it is same for beam  $B_2$  )

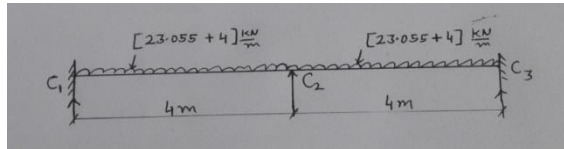
	DL	LL
from slab portion (hatched)	[ 4.125 + 4.0 ] $\text{kn/m}$	
{ $0.5*4*2 [ 4.125 + 4.0 ] \text{kn/m}^2$ }		
load per unit length of beam is [4.125 + 4.0] $\text{kn/m}$		
from masonry wall with plaster	[15.555 + 0.0 ] $\text{kn/m}$	
{ $20\text{kn/m}^3 * (3.5-.45)\text{m}*(0.23+2*0.0125)\text{m}$ }		
Beam self weight	[ 3.375 + 4.0 ] $\text{kn/m}$	
{ $25\text{kn/m}^3*0.3\text{m}*0.45\text{m}$ }		
Sum =	[ 23.055 + 4.0 ] $\text{kn/m}$	

(C) Load taken by Beam  $B_7$

(In our case it is same for beam  $B_{11}$ )

DL	LL
[ 23.055 + 4.0 ] $\text{kn/m}$	

( D ) By beam reaction method



	DL	LL
Load on $C_1 = \frac{1}{2} [ [ 23.055 + 4 ] \text{ kN/m} * 4\text{m} ]$	[ 46.11	+ 8 ] kn
Load on $C_2 = 2 * \frac{1}{2} [ [ 23.055 + 4 ] \text{ kN/m} * 4\text{m} ]$	[ 92.22	+ 16] kn

Note : Due to similarity of our structure , load transferred to  $C_1$  from beam  $B_7$  is same as that for beam  $B_1$ . Likewise , load transferred to  $C_3$  from beam  $B_{11}$  is same as that for beam  $B_2$  .

(E) Load taken by beam  $B_9$

(i) from hatched terrace portion

$2 * ( \frac{1}{2} * 4 * 2 ) \text{m}^2 * [ 4.125 + 4 ] \text{ kN/m}^2$	DL	LL
= [33 + 32 ]kn	[ 8.25	+ 8.0 ]kn/m

load per unit length of beam is [8.25 + 8.0]kn/m

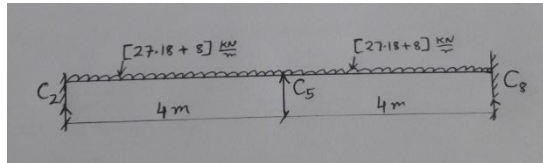
(ii) from masonry wall with plaster

$20 \text{ kN/m}^3 * (3.5 - 0.45) \text{m} * ( 0.23 + 2 * 0.0125 ) \text{m}$	[ 15.555	+ 0.0 ] kn/m
= 15.555 kn/m		

(iii) beam self weight

$25 * 0.3 * 0.45 = 3.375 \text{ kN/m}$	[ 3.375	+ 0.0 ] kn/m
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Sum =	[ 27.18	+ 8.0 ] kn/m
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(F) Load on column  $C_2$  from beam  $B_9$

$\frac{1}{2} [ 27.18 + 8.0 ] \text{ kN/m} * 4\text{m}$	=	[ 54.36 + 16.0 ] kn
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**Load calculation for column  $C_1$  ,  $C_2$  &  $C_3$  of one story**

	Load from hori. grid beam $B_1$	Load from vert. grid beam $B_7$	Col. Self weight $25 * .5 * .5 * (3.5 - 0.45)$	Total Load
Col. $C_1$	DL      LL [ 46.11   +   8.0 ] kn	DL      LL [ 46.11   +   8.0 ] kn	DL      LL [ 19.06   +   0.0 ] kn	DL      LL [ <b>111.28</b> + <b>16.0</b> ]
Col. $C_2$	DL      LL [ 92.22   +   16.0 ] kn	DL      LL [ 54.36   +   16.0 ] kn	DL      LL [ 19.06   +   0.0 ] kn	DL      LL [ <b>165.64</b> + <b>32.0</b> ]
Col. $C_3$	DL      LL [ 46.11   +   8.0 ] kn	DL      LL [ 46.11   +   8.0 ] kn	DL      LL [ 19.06   +   0.0 ] kn	DL      LL [ <b>111.28</b> + <b>16.0</b> ]

**Axial load on column C<sub>1</sub> and C<sub>3</sub> due to DL & LL for load combination (DL +LL +EL)**

Floor	Loads in KN		TL	Cumulative		
	DL	50% of LL		DL	LL	TL
5 <sup>th</sup>	111.28	8	119.28	111.28	8	119.28
4 <sup>th</sup>	111.28	8	119.28	222.56	16	238.56
3 <sup>rd</sup>	111.28	8	119.28	333.84	24	357.84
2 <sup>nd</sup>	111.28	8	119.28	445.12	32	477.12
1 <sup>st</sup>	111.28	8	119.28	556.40	40	596.40
G.F.	111.28	8	119.28	667.68	48	715.68
Foundation	19.75	0	19.75	687.42	48	<b>735.43</b>

Note : Loads on columns between GF and footing include self weight of ground beams and self weight of column from ground beam to the top of footing. Ground floor use for parking so no walls.

**Axial load on column C<sub>2</sub> due to DL and LL for combination ( DL +LL+EL )**

Floor	Loads in KN		TL	Cumulative		
	DL	50% of LL		DL	LL	TL
5 <sup>th</sup>	165.64	16	181.64	165.64	16	181.64
4 <sup>th</sup>	165.64	16	181.64	331.28	32	363.28
3 <sup>rd</sup>	165.64	16	181.64	496.92	48	544.92
2 <sup>nd</sup>	165.64	16	181.64	662.56	64	726.56
1 <sup>st</sup>	165.64	16	181.64	828.20	80	908.20
G.F.	165.64	16	181.64	993.84	96	1089.84
Foundation	26.50	0	26.50	1020.34	96	<b>1116.34</b>

Total Seismic weight  $W = W_1 + W_2 + W_3$

$W = 735.43 + 1116.34 + 735.43$

$W = 2587.2 \text{ KN}$

As  $V_B = 0.0346 W$  , thus  $V_B = 0.0346 * 2587.2 = 89.517 \text{ KN}$

The base shear  $V_B$  will be now distributed at each storey . The calculations are tabulated in table below .

Level	$W_i$	$h_i$	$W_i h_i^2$	$Q_i = V_B \frac{W_i h_i^2}{\sum W_i h_i^2} = 89.517 * \frac{W_i h_i^2}{\sum W_i h_i^2}$
Roof	420.20	22.45	$211.781 \times 10^3$	$Q_{6-6} = 34.274 \text{ kn}$
5 <sup>th</sup> floor	420.20	18.95	$150.895 \times 10^3$	$Q_{5-5} = 24.42 \text{ kn}$
4 <sup>th</sup> floor	420.20	15.45	$100.302 \times 10^3$	$Q_{4-4} = 16.23 \text{ kn}$
3 <sup>rd</sup> floor	420.20	11.95	$60.005 \times 10^3$	$Q_{3-3} = 9.71 \text{ kn}$
2 <sup>nd</sup> floor	420.20	8.45	$30.003 \times 10^3$	$Q_{2-2} = 4.856 \text{ kn}$
1 <sup>st</sup> floor	420.20	4.95	$10.296 \times 10^3$	$Q_{1-1} = 1.666 \text{ kn}$
G.F.	66.00	1.45	$0.1388 \times 10^3$	$Q_{g-g} = 0.022 \text{ kn}$

Nodes are considered at the centre of beam – column joint .

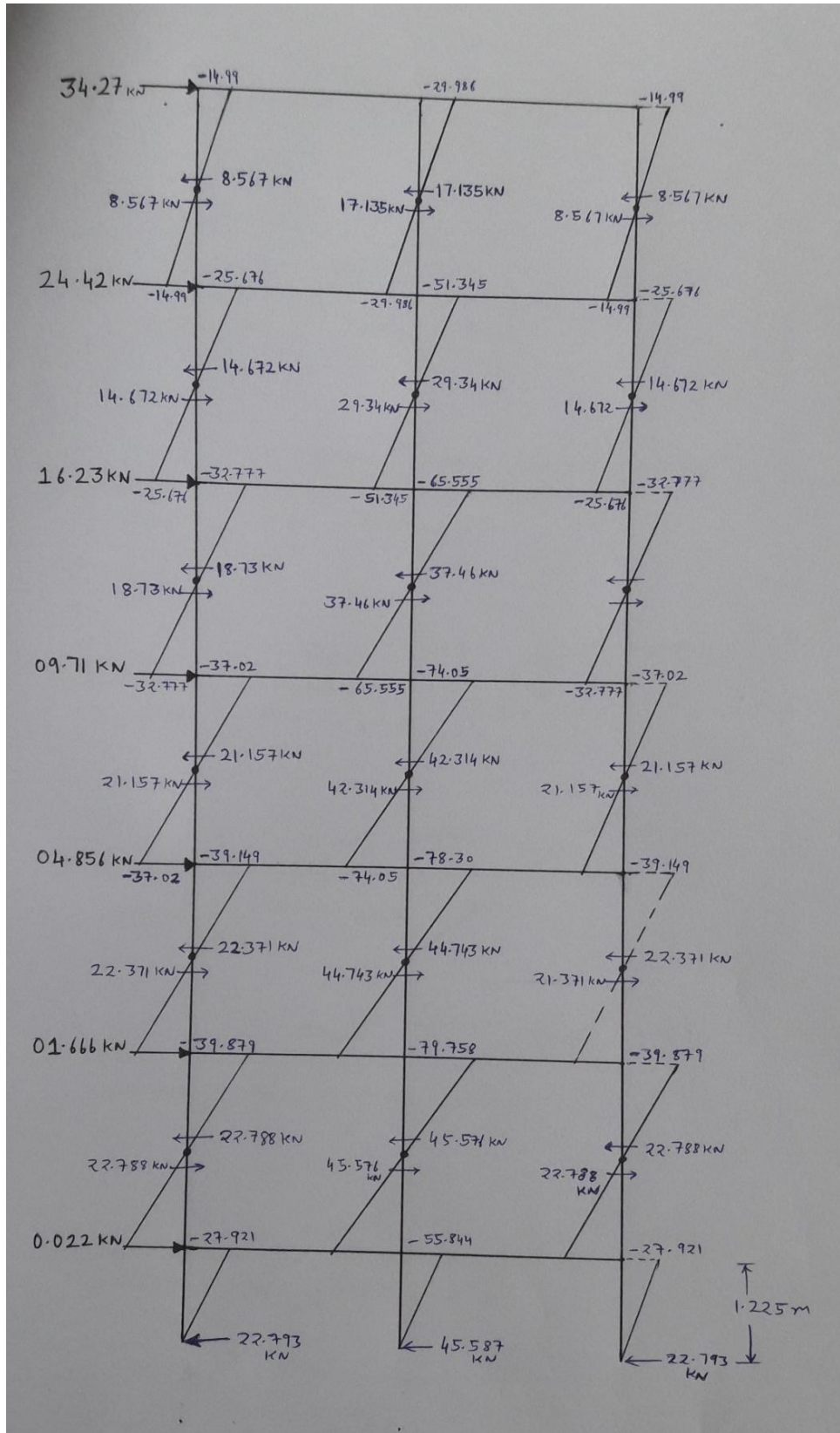


Diagram showing columns shear and moment for external frame C<sub>1</sub> - C<sub>2</sub> - C<sub>3</sub>

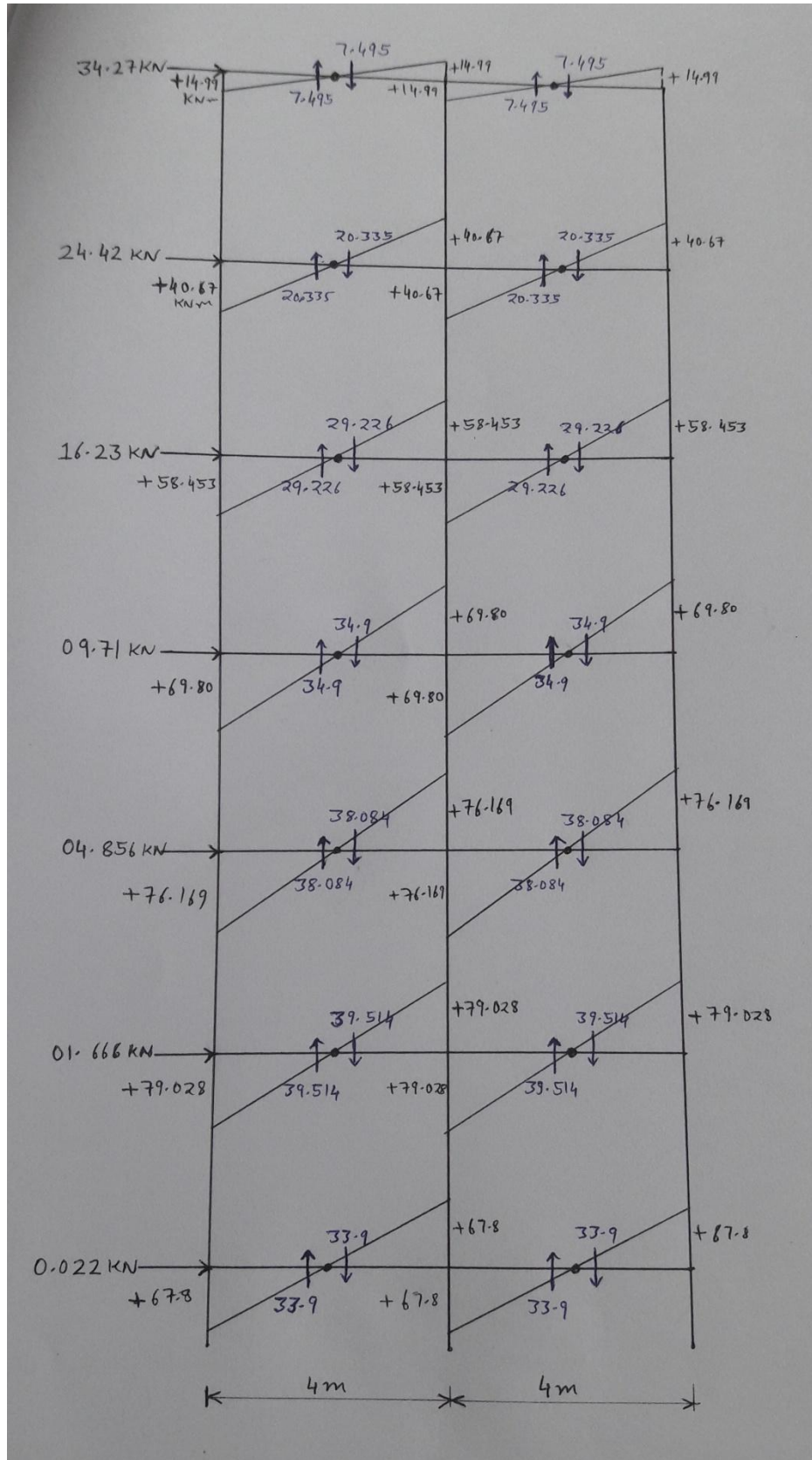


Diagram showing girders moment and shear for external frame C<sub>1</sub> - C<sub>2</sub> - C<sub>3</sub>

## **5.CONCLUSION**

We have done seismic analysis manually. By Analyzing this building , we have gained clarity and knowledge about the earth quake effects . Actually while doing manual calculations, we have gained more knowledge than analyzing using software. By doing this project we have become more familiar with standard codes . We have felt the real engineering practice in this work .

## **6.ACKNOWLEDGEMENT**

My sincere thanks to my department colleagues for their constraint help during my research .

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